

AN ADDITION TO OPTIMIZATION OF PARAMETERS IN Ti-ALLOYS

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ABSTRACT

Due to its characteristics, titanium is a material that engineers increasingly use and many call it a material of the future. Fields of application are not closely confined to air and missile industry, but have spread to almost all spheres of human creation. The limiting factor is still the price of titanium. Previous workability studies of Ti-alloys grinding finish do not provide sufficient answers in which area (which parameters) processing should be done. Although, essentially, the process of grinding, can be reduced to the classical process, it still contains many undetermined factors, so that the empirical and theoretical data of different authors differ greatly.

Keywords: Ti-alloys, machining, grinding

1. INTRODUCTION

According to demands of modern production and a techno-economic analysis of treatment operations, treatment process project should include a defining of optimal parameters in order to reduce both the costs and production time.

The parameters need to provide a predefined quality nad process cost-effectiveness. The starting point are technological and technical demands whenever treatment parameters are determined in regards to rigidity and efficiency of installed power of the treatment system.

Many significant parameters influence roughness of the treated surface (Fig. 1). By managing those parameters, it is possible to get necessary values of roughness (R_a , R_z , R_{max}). The real resting surface depends on roughness and treatment procedure so for the asperity height of $2,5\div 8\ \mu\text{m}$ (grinding) the contact surface is 10%; for the height of $0,8\div 2,5\ \mu\text{m}$ the resting surface is 40%, whereas for fine treatment (fine grinding) the resting surface is up to 90%.

The paper provides comparative values of roughness of a Č.1530 i TA6V sandwich construction.

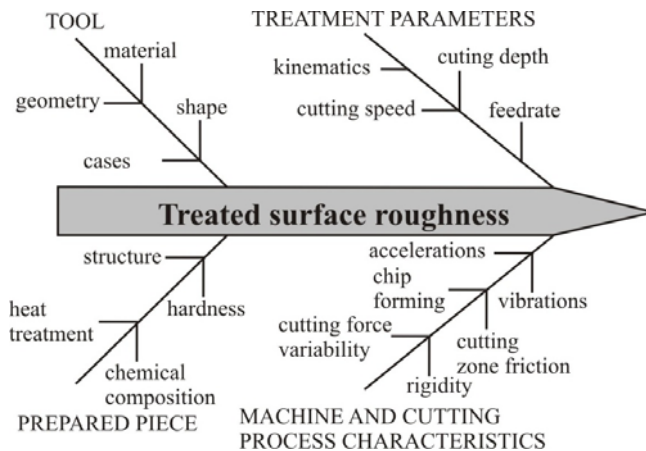


Figure 1. Influence parameters to the roughness of the treated surface

2. EXPERIMENT CONDITIONS OF DETERMINING OF TREATED SURFACE QUALITY OF A Č.1531-TA6V SANDWICH CONSTRUCTION

2.1. MATERIAL

The tube material (sandwich construction) is commercial steel, made by hot rolling. The material is then thermally treated by means of normalizing and annealing, and the other material is an alloy.

Table 1. Mechanical characteristics and chemical composition of the tube material

Č.1331 BAS Cg 32 DIN 1.0612 WNr	Mechanical characteristics						
	Ultimate strength N/mm ²	Stretch limit N/mm ²	Hardness HB	Ductility A ₅ %	Contraction %		
	650	420	179	24,2	48,2		
	Chemical composition %						
	C	Si	Mn	P	S	Ni	Mo
0,467	0,309	0,657	0,0141	0,0211	0,0339	0,0087	
Titanium alloy T-A6V	Mechanical characteristics						
	Ultimate strength N/mm ²	Stretch limit N/mm ²	Hardness HB	Ductility A ₅ %			
	400-900	500-600	200-220	20-25			
	Chemical composition %						
	Al	V	Fe	C	N ₂	O ₂	Ti
6,87	4	0,13	0,08	0,07	0,02	Other	

2.2. Tube Shape



Sl.2. Tube shape

2.3. Tool - Whetstone

We used a whetstone labeled 2B 46 J 6V, manufacturer “SWATY”, Tovarna umjetnih brusov, ISO 525. Whetstone dimensions $\phi 250 \times 35 \times 26$.

2.4. Measuring Spot

Surface roughness measuring device – profilometer. In order to acquire data on the quality of the treated surface, we used a Surface roughness measuring device (R_a , R_z , R_{max}) manufacturer Mitutoyo, labeled SJ-201P, of the referential length of 2,5 mm.

3. EXPERIMENT RESULTS

Table 2. The result of measuring of the quality of sandwich construction treated surface

	Table feedrate s [mm/o]	Cutting depth t [μm]	Table speed v [m/min]	X_0	X_1	X_2	X_3	Č.1530			TA6V		
								R_a [μm]	R_a Computer	$\ln R_a$	R_a [μm]	R_a Computer	$\ln R_a$
13	4	0,015	10	1	1	1	1	0,65	1,1623	-0,43	1,37	1,427769	0,31
10	1	0,015	10	1	-1	1	1	1,30	1,2200	0,26	1,90	1,954877	0,64
6	4	0,005	10	1	1	-1	1	0,78	0,6583	-0,25	0,75	1,00165	-0,29
15	1	0,005	10	1	-1	-1	1	0,62	0,6910	-0,48	1,57	1,371442	0,45
4	4	0,015	2	1	1	1	-1	1,40	1,0169	0,34	1,90	1,846008	0,64
1	1	0,015	2	1	-1	1	-1	0,95	1,0673	-0,05	2,30	2,527522	0,83
2	4	0,005	2	1	1	-1	-1	0,40	0,5760	-0,92	1,40	1,295065	0,34
5	2	0,008	4,47	1	0	0	0	1,00	0,8382	0,00	1,80	1,666714	0,59
3	1	0,005	2	1	-1	-1	-1	0,45	0,6045	-0,80	1,40	1,773181	0,34
8	2	0,008	4,47	1	0	0	0	1,10	0,8382	0,10	1,60	1,666714	0,47
12	2	0,008	4,47	1	0	0	0	1,00	0,8382	0,00	1,90	1,666714	0,64
14	2	0,008	4,47	1	0	0	0	1,10	0,8382	0,10	1,80	1,666714	0,59

The results gained from the Table 2. give us:

$$R_a = \frac{8,85 \cdot t^{0,51743} \cdot v^{0,08306}}{s^{0,0349}} [\mu m] \quad \text{Č.1530}$$

$$R_a = \frac{10,95 \cdot t^{0,32265}}{s^{0,2267} \cdot v^{0,1596}} [\mu m] \quad \text{TA6V}$$

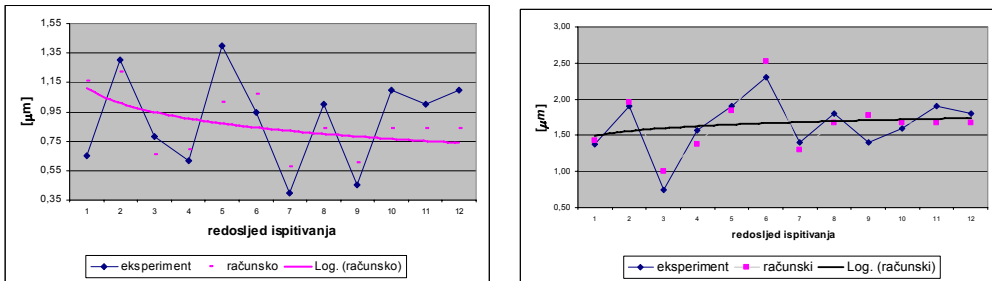


Figure 3. An overview of computer-generated and experimental results of roughness R_a - Č.1530 and R_a - TA6V

4. CONCLUSION

Based on the technological knowledge and conducted experiments of sandwich construction titanium alloy TA6V and Č.1530 grinding, we can conclude that:

- Input parameters optimization (cutting speed, feedrate and cutting depth) on the basis of set treatment limitations (machine and tool characteristics and accuracy of the treated surface), and with the goal of achieving one or more functions of the goal, such as minimization of unit treatment costs and/or minimization of unit treatment time, as well as an application of material workability criteria, have, from cost efficiency point of view, have the largest practical value and meaning in the production environment.
- It is noticeable that tools with recommended workability characteristics have a significantly lower consistency than in case of grinding conventional materials.
- Of all cutting parameters for all cases of testing, feedrate has the biggest influence, whereas, on the contrary, speed has very little influence on the resistance and roughness parameter R_a .
- While analyzing parameters R_a it is noticeable that the roughness of the treated surface is mostly formed under the influence of geometrical influences related to the tools and feedrate, while the influence of elastic-plastic deformities is minimal.

5. REFERENCES

- [1] Haznadarević L., Mišković A.: „Appendix to the study of thermal condition by process of grinding”, Naučni skup “MATRIB '05”, Vela Luka, 2005.
- [2] Kevelj J., Haznadarević L.: „Contribution to Studies in Grinding Machining Ti Alloys”, 14th International Research/Expert Conference ”Trends in the Development of Machinery and Associated Technology” TMT 2010, Mediterranean Cruise, 11-18 September 2010.
- [3] Haznadarević L., Kevelj J.: „Optimalno područje brušenja titanovih legura”, 3rd International Conference on Computer Aided Design and Manufacturing CADAM 2005, September 27th – October 1st 2005, Supetar – Brač, Croatia.
- [4] Ekinović S.: Postupci obrade rezanjem, Univerzitet u Sarajevu, Mašinski fakultet u Zenici, Zenica, 2003.
- [5] Jurković Z.: Modeliranje i optimizacija parametara obrade primjenom evolucijskih algoritama kod inteligentnih obradnih sustava, Doktorska disertacija, Tehnički fakultet Rijeka, Rijeka, odbranjena 09. 10. 2007.
- [6] Ekinović S.: Metode statističke analize u Microsoft EXCEL-u, Mašinski fakultet u Zenici Univerziteta u Sarajevu, Zenica, 1997.