

FINITE ELEMENT ANALYSIS OF SHELL-TYPE STRUCTURES WITH OPENINGS BASED ON THE PROJECTIVE-ITERATIVE SCHEMES

Hart E. L.

Oles Honchar Dnepropetrovsk National University
Gagarin av., 72, 49010, Dnepropetrovsk
Ukraine

Hudramovych V. S.

Institute of Technical Mechanics of National Academy of Sciences Ukraine
and State Space Agency Ukraine
Leshko-Popel st., 15, 49005, Dnepropetrovsk
Ukraine

Ryabokon' S. A.

Institute of Technical Mechanics of National Academy of Sciences Ukraine
and State Space Agency Ukraine
Leshko-Popel st., 15, 49005, Dnepropetrovsk
Ukraine

Samarskaya E. V.

Institute of Technical Mechanics of National Academy of Sciences Ukraine
and State Space Agency Ukraine
Leshko-Popel st., 15, 49005, Dnepropetrovsk
Ukraine

ABSTRACT

Based on the projective-iterative versions (PIV) finite element method (FEM) calculation schemes developed for determining the stress-strain state of shell-type structures with openings. Cutouts (discontinuities) characterize the design features or are damage defects and appear in various situations of exploitation. Plastic deformation of the material is taken into account when using the method of elastic solutions that reduce the solution of elastoplastic problems to solution of elastic problems. Developed PIV significant savings of computer calculation, compared with the traditional FEM (calculated on a fine mesh). Designed scheme allows analysis of the mutual influence of openings. The analysis of the transformation zone of plastic deformation is developed. For definiteness, the cylindrical shell structures with several rectangular openings is considered.

Keywords: finite element method, projective-iterative schemes, shell structures, opening, elastoplastic deformation

1. INTRODUCTION. FORMULATION OF PROBLEM

The shell-type structures are optimal combination of necessary strength and minimum weight. Structures of modern techniques have often openings of various types. Cutouts (discontinuities) characterize the design features or are damage defects and appear in technological manufacturing processes or in various situations of exploitation. They reduce to concentration of stresses.

Such structures are relevant to the priority areas of technology (aviation, space technology, oil and gas industry, etc.) [1, 2].

High load levels lead to plastic deformation. This fact taken into account when using the method of elastic solutions that reduce the solution of elastoplastic problems to solution of elastic problems [3].

The fields of stresses and strains that arise near openings' edges have the mutual influence on each other. This influence depends on the openings' shape, dimensions, quantity, and spacing. Plastic deformation appreciably changes the pattern of this interaction. Transformation of above-mentioned fields near the openings cause changes to the process of exhausting the carrying capacity.

The plastic deformation zones, stress distributions, loads that correspond to the start of merging and further transformation in the course of loading make it possible to predict load-carrying ability of shell-type structures with openings.

Let us consider shell-type structures with rectangular openings. For concreteness, consider a cylindrical shell with three openings.

2. FEATURES OF USED SOLUTION METHODS

The numerical finite element method (FEM) is an efficient method for solution of various complex problems of deformation and critical states (carrying capacity, stability) of such structures.

The projective-iterative versions (PIV) of FEM essentially reduces the needed for calculations performed by means of personal computers, which is of importance in simulation of complex nonlinear deformation of shell-type structures with openings of various types.

The theoretical foundations of PIV FEM in [4-7] and in series of works in mathematics problems are presented. The basic idea is as follows.

The problem of finding the minimum of the potential energy functional, defining the stress-strain state of shell structure members is the conditional minimization problem

$$I[z] \rightarrow \inf, \quad z \in Z, \quad (1)$$

where $I[z]$ is the functional bounded on a set of cinematically possible displacements Z of the real Hilbert space.

The extremum problem (1) is approximated, through the use of FEM, by a series of discrete extremum problems ($n = 1, 2, \dots$). Each of the problem is solved via some iterative process, but not completely. Starting from an arbitrary rather rough breakdown of the mesh, one constructs just a few approximations (k_n) to the minimum point of the n th multivariable function. The last approximation is interpolated into a finer finite element mesh and serves an initial approximation to the minimum point of the next function at the $(n+1)$ th step of the PIV process that goes on until a present calculation accuracy is achieved.

The PIV FEM models have been applied successfully of elastic boundary value problems, elastoplastic stress-strain state problems for plates with various openings, plane elastoplastic deformation problems for structured media containing assemblies of pores, cracks, inclusions [2, 7]. Use of this models provides a significant (dozens - fold) saving in computation time in comparison to the conventional FEM.

For solution of elastoplastic problems we use the method of variable elastic parameters (VEP) – version of elastic solutions methods [3, 7]. The method give construction of iterative process, in each approximation an elasticity problem with variable shear modulus G' , modulus of elasticity E' and Poisson's ratio ν' is solved. For deformation theory we have for each approximation

$$\varepsilon_{ij} = \frac{(1+\nu')\sigma_{ij} - 3\nu'\sigma\delta_{ij}}{E'}, \quad (2)$$

$$E' = 2G'(1+\nu'); \quad G' = \frac{1}{2\psi}; \quad \nu' = \frac{E\psi - 1 + 2\nu}{2E\psi + 1 - 2\nu}; \quad \psi = \frac{3\varepsilon_i}{2\sigma_i},$$

where σ_{ij} and ε_{ij} are the components of stresses and strains tensors, σ_i and ε_i are the stress and strain intensities, σ is the mean stress, δ_{ij} is the Kronecker delta.

For a first approximation, we set $E'_1 = E$, $v'_1 = v$ and determine σ_{ij1} , σ_{i1} , ε_{i1} , ψ_1 . In a second approximation we have $E'_2 = \sigma_{i1}/\varepsilon_{i1}$, v'_2 (2) at ψ_1 and so on. The process is run until two successive approximations coincide to within a given accuracy, $E'_m \approx E'_{m-1}$.

Corresponding schemes for the flow theory may be constructed.

The corresponding minimized energy functional for shell with openings is written as [8]

$$I = h \iint_{\Omega} \frac{G'}{1-v'} \left[u_{,\alpha}^2 + 2v' u_{,\alpha} \left(v_{,\beta} + \frac{w}{R} \right) + \left(v_{,\beta} + \frac{w}{R} \right)^2 + \frac{1}{2} (1-v') (u_{,\beta} + v_{,\alpha})^2 \right] d\alpha d\beta +$$

$$+ \frac{h^3}{12} \iint_{\Omega} \frac{G'}{1-v'} \left[w_{,\alpha\alpha}^2 + 2v' w_{,\alpha\alpha} \left(w_{,\beta\beta} - \frac{v_{,\beta}}{R} \right) + \left(w_{,\beta\beta} - \frac{v_{,\beta}}{R} \right)^2 + 2(1-v') \left(w_{,\alpha\beta} - \frac{v_{,\alpha}}{R} \right)^2 \right] d\alpha d\beta -$$

$$- \int_{\Gamma} (T_1 u + S_1 v + Q_1 w + M_1 \phi_1) d\beta, \quad (4)$$

where u , v , and w are the displacements of the middle surface, α and β - coordinates, h is the shell thickness, Ω is the sheet surface, G' and v' are the variable elastic parameters for each method VEP approximation, T_1 , S_1 , Q_1 and M_1 are the longitudinal, tangential, transverse force and bending moment, respitively which are applied to the shell edges Γ , comma denotes differentiation in the coordinate. Stresses in the shell middle surface are given by

$$\sigma_{\alpha} = \frac{2G'}{1-v'} \left[u_{,\alpha} + v' \left(v_{,\beta} + \frac{w}{R} \right) \right], \quad \sigma_{\beta} = \frac{2G'}{1-v'} \left(v_{,\beta} + \frac{w}{R} + v' u_{,\alpha} \right), \quad \sigma_{\alpha\beta} = G' (u_{,\beta} + v_{,\alpha}). \quad (5)$$

The strain intensity is determined by the formula

$$\varepsilon_i = \frac{2}{3} \left[\frac{\left((1-v' + v'^2) \left(u_{,\alpha} + v_{,\beta} + \frac{w}{R} \right)^2 \right)}{(1-v')^2} - 3u_{,\alpha} \left(v_{,\beta} + \frac{w}{R} \right) + \frac{3}{4} (u_{,\alpha} + v_{,\beta})^2 \right]^{\frac{1}{2}}.$$

3. RESULTS OF NUMERICAL ANALYSIS

Founded on the PIV FEM procedure, a program in C++ language has been written for the stress-strain state analysis of cylindrical shell with three rectangular openings. We studied shells ($L=1.6$ m, $R=1$ m and $h=0.004$ m) of D16T aluminum alloy (Fig. 1). The larger openings measures 0.4×0.4 m and the smaller one 0.2×0.2 m. Compressive loads p were varied from 60 to 90 MPa. The center-to-center distances: l_1 - between the small opening and the nearest larger opening, l_2 - between two larger openings were varied. The offset yield stress σ_s was taken 200 MPa.

The PIV FEM has been implemented on eight double-folded FE meshes of rectangular Hermitian elements. The number k_n of approximations at the n th step ($n=1, 2, \dots, 8$) of the PIV process was chosen as the smallest integer k satisfying the condition

$$\left\| z_n^{(k)} - z_n^{(k-1)} \right\| \leq \varepsilon_n, \quad k=1, \dots, k_n, \quad (6)$$

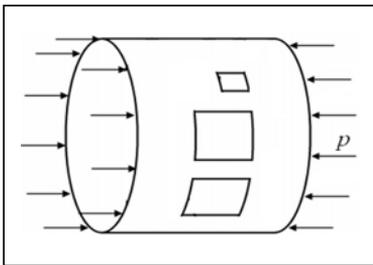


Figure 1. Loading scheme of shell

where $z_n^{(k_n)}$ is the solution to the n th finite-dimensional problems and ε_n is the preset accuracy of computations on the n th mesh.

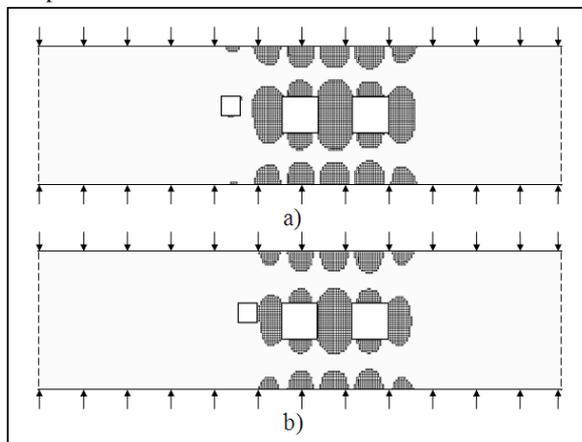


Figure 2. Distribution of plastic strain zones in a shell with openings

Let us consider some results of the numerical analysis.

By way of plane projections of the shell evolvent, Fig. 2 shows how the plastic strain zones develop in a shell with three openings: $l_1 = l_2 = 0.8$ m, $p = 45$ MPa (Fig. 2a); $l_1 = 0.6$ m, $l_2 = 0.8$ m, $p = 35$ MPa (Fig. 2b).

These zones arise locally at the openings edges and at shell ends, merge as the load p grow and l decreases. The variants of mutual influence of the openings will differ as the shell and openings parameters are changed.

Using the computation program we can determine the loads whereby the plastic strain zones start merging to be become integral ones. The use PIV FEM models in these problems has provided a saving

of computer time by a factor of 30 to 50 (depending on the class of problems) in comparison to the traditional FEM models (on a single mesh).

The plastic strain zones affect stiffness. The formation of the zones common for the openings considerably impairs the resistance of shall-type structures with openings to effective loads. This finding can be used in predicting their load-carrying capacity.

4. CONCLUSION

Founded on PIV FEM models that significantly reduce the computation time (in comparison to the conventional FEM models – on a single mesh), stress-strain analysis methods and algorithms for elastoplastic shell-type structures containing several rectangular openings are developed. The variation of openings parameters, quantity, and center-to-center distances allows one to study the formation and transformation of plastic strain zones in the process of loading. Merging of the zones leads to a decrease in stiffness; this fact is used in predicting the load-carrying capacity.

5. REFERENCES

- [1] Preobrazhenskii I., Tsurpal I.: Openings in supporting structures [in Russian]. Mashinostrojenie, Moscow, 1984.,
- [2] Hart E., Hudramovich V.: Applications of the projective-iterative versions of FEM in problems of damage for engineering structures. Proc. Second International Conference Maitanance 2012 (Zenica, Bosnia and Herzogovina), Zenica, 2012.,
- [3] Il'yushin A.: Collected works in 4 volumes, Vol. 2: Plasticity: 1946-1966 [in Russian]. Fizmatlit, Moscow, 2004.,
- [4] Krasnosel'skii M., et al.: Approximate solution of operator equations [in Russian]. Nauka, Moscow, 1969.,
- [5] Kluge R.: Ein Projektions-Iterationsverfahren bei Fixpunktproblemen und Gleichungen mit monothonen Operatoren, Monatsber. Dtsch. Akad. Wissenschaft, Berlin, 8-9, 1969.,
- [6] Shaidurov V.: Multigrid finite element methods [in Russian]. Nauka, Moscow, 1978.,
- [7] Hudramovich V., Hart E., Ryabokon' S.: Elastoplastic deformation of nonhomogeneous plates. Journal of Engineering Mathematics, Issue 1, 2013.,
- [8] Novozhilov V., Chernych K., Michailovskii E.: Linear theory of thin shells [in Russian]. Politehnika, Leningrad, 1991.